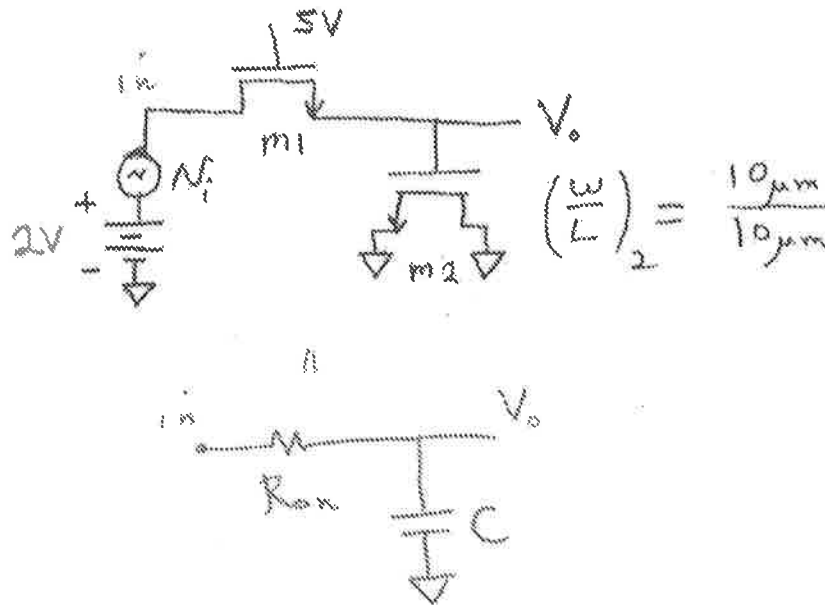


5.16

1. A first-order RC filter that uses only MOS transistors is shown below. Assume that the AC input signal is small compared to the DC input bias voltage. What W/L ratio is needed for M1 to give a -3 dB frequency of 10 MHz? Ignore all junction and overlap capacitances.



$$C = C_{gs}(m_2) = C_{ox} \cdot W \cdot L = 3.5 \text{ fF}/\mu\text{m}^2 \times 10\mu\text{m} \times 10\mu\text{m} = 350 \text{ fF}$$

m_1 trade:

$$R_{on} = \frac{1}{\mu C_{ox} \frac{W}{L} (V_{GS} - V_T)} = \frac{1}{180 \frac{\text{A}}{\text{V}^2} \left(\frac{W}{L}\right) [5 - 2 - 1] \text{V}}$$

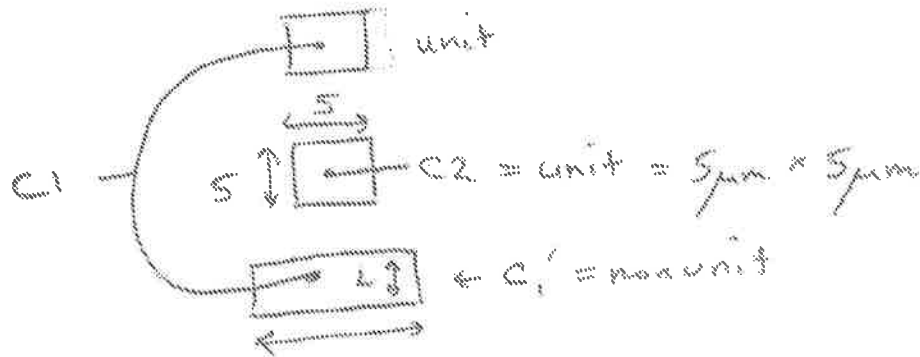
$$= \frac{2778 \Omega}{\frac{W}{L}}$$

want $\frac{1}{2\pi R_{on} C} = 10 \text{ MHz} \Rightarrow R_{on} = 45.5 \text{ k}\Omega$

$$\Rightarrow \frac{W}{L} = 0.061$$

6

2. Two capacitors C_1 and C_2 are needed with a very accurately defined ratio of $C_1/C_2 = 2.6$, with the constraint that the maximum area that can be used for C_2 is $25 \mu\text{m}^2$. Draw a top view of the layout of the two capacitors. Show the dimensions of the capacitors on your drawing.



$$C_2 = \text{biggest unit cap possible} = 5 \mu\text{m} \times 5 \mu\text{m}$$

$$C_1 = 1 \text{ unit} + 1 \text{ non unit}$$

$$C_1' = \text{nonunit} : \text{area} = wL = 1.6 (25 \mu\text{m}^2) = 40 \mu\text{m}^2$$

||
w · L

$$\frac{\text{per}}{\text{area}} (C_1') = \frac{\text{per}}{\text{area}} (\text{unit})$$

$$\frac{20 \mu\text{m}}{25 \mu\text{m}} \Rightarrow w + L = \frac{20}{25} (40) \cdot \frac{1}{2} = 16 \mu\text{m}$$

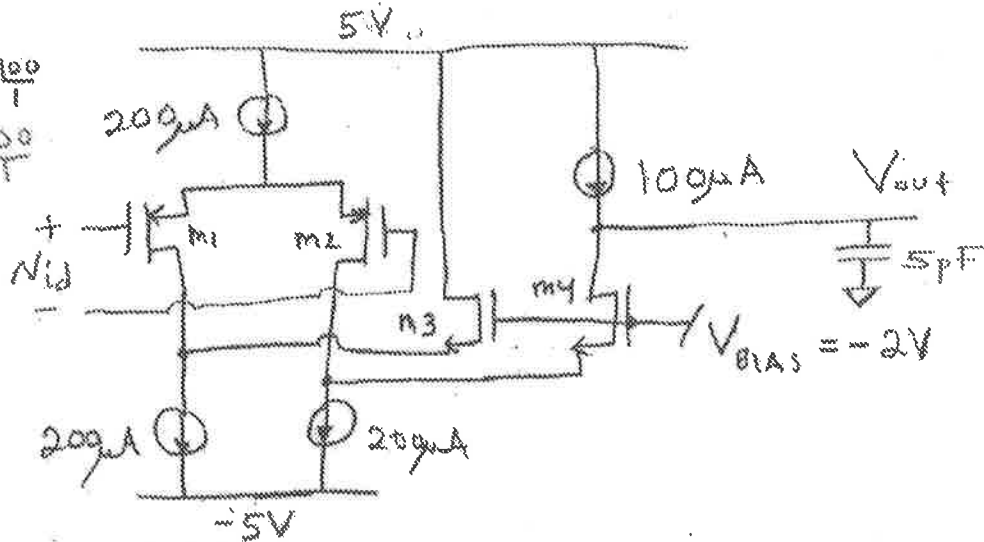
$$w + L = w + \frac{40}{w} = 16 \Rightarrow w = 12.9 \mu\text{m}$$

$$\frac{40}{w} = 3.1 \mu\text{m}$$

3. For the op amp shown below, assume DC biasing places the transistors in the saturation region. (NOTE: This op amp is slightly different than the standard folded-cascode op amp.)

$$m_1 = m_2: \frac{W}{L} = \frac{100}{1}$$

$$m_3 = m_4: \frac{W}{L} = \frac{100}{1}$$



⑤

a) What is the low-frequency gain? $v_{out}/v_{id} =$ _____

$$a_v = \frac{1}{2} g_{m2} R_{out+} = \frac{1}{2} (1100 \frac{\mu A}{V}) (950 m\Omega) = \underline{\underline{522}}$$

$$g_{m2} \approx \sqrt{2 (60 \frac{\mu A}{V}) (100) (100 \mu A)} = 1100 \frac{\mu A}{V}$$

$$R_{out+} = r_{o4} (1 + g_{m4} r_{o2}) = 90k \Omega [1 + (1900 \frac{\mu A}{V}) (1m\Omega)] = 950m\Omega$$

$$r_{o4} = \frac{1}{0.02 \cdot 100 \mu A} = 500k\Omega$$

$$g_{m4} = \sqrt{2 (180 \frac{\mu A}{V}) (100) (100 \mu A)} = 1900 \frac{\mu A}{V}$$

$$r_{o2} = \frac{1}{(0.01 \frac{\mu A}{V}) (100 \mu A)} = 1m\Omega$$

②

b) What is the positive output slew rate? $SR^+ =$ _____

$$\frac{dV_{out}}{dt} = \frac{100 \mu A}{5pF} = \underline{\underline{20 \times 10^6 \frac{V}{s}}}$$

③

c) What is the dominant pole for this op amp? $p_1 =$

$$p_1 \approx \frac{-1}{R_{out} C_L} = \frac{-1}{(950 \text{ m}\Omega)(5 \text{ pF})} = -210 \frac{\text{rad}}{\text{s}}$$

③

d) Estimate the frequency at which the magnitude of the voltage gain falls to one. Ignore the nondominant poles for this calculation. (This is the GBW.) $f_u =$ 17.5 MHz

$$a_{v_0} \cdot |p_1| = 1 \cdot \omega_u$$

$$(522 \text{ k})(210 \frac{\text{rad}}{\text{s}}) = \omega_u = 110 \text{ M} \frac{\text{rad}}{\text{s}}$$

||
 $2\pi f_u$

③

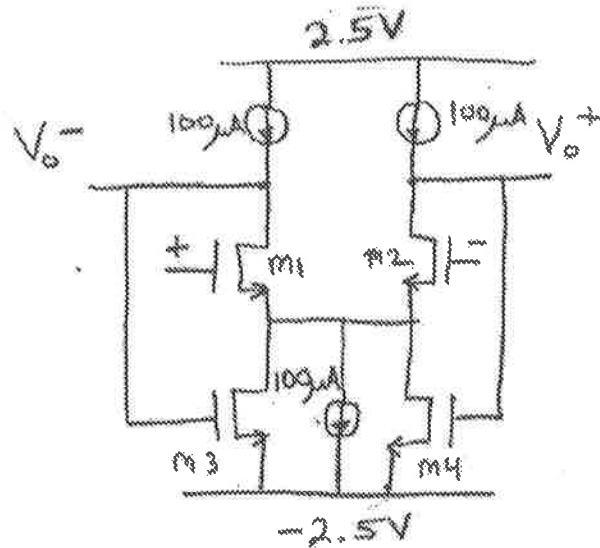
e) Estimate the negative output swing limit.

Negative output swing limit = _____

can swing down until m_4 goes triode
(when $V_{GS}(m_4) = V_T = 1 \text{ V}$)

$$V_o^- = -2 \text{ V} - V_{GS}(m_4) = -2 \text{ V} - 1 \text{ V} = \underline{\underline{-3 \text{ V}}}$$

4. A fully differential one-stage op amp with common-mode feedback is shown. The common-mode feedback is provided by M3 and M4. Assume all transistors are saturated, and assume $M1 = M2$, $M3 = M4$.



$$M1 = M2: \frac{W}{L} = 100$$

$$M3 = M4$$

④

a) What should W/L be for $M3$ and $M4$ so that the common-mode output voltage is $0V$?

$$W/L = \underline{\hspace{2cm}}$$

$$\text{Want } I_{D3} = I_{D4} = 50\mu A = \frac{1}{2} \left(180 \frac{\mu A}{V^2} \right) \frac{W}{L} \left(0 - (-2.5V) - 1V \right)^2$$

$$\frac{W}{L} = \underline{\underline{0.25}}$$

④

b) What is the differential-mode (DM) voltage gain?

$$v_{od}/v_{id} = \underline{\hspace{2cm}}$$

$$A_v = g_{m1} r_{o1} = \sqrt{2 \left(180 \frac{\mu A}{V^2} \right) (100) (100\mu A)} \times \frac{1}{0.52V^{-1} \cdot 100\mu A}$$

$$= \underline{\underline{950}}$$

④

c) For this op amp, estimate the lower limit of the common-mode input voltage.

Lower CM input limit = _____

limit when M_3 goes triode:

$$V_{in}^- (CM) = -2.5V + V_{DSAT}(M_3) + V_{GS}(M_1)$$

$$= -2.5V + \sqrt{\frac{2I_{D3}}{\mu C_{ox} \frac{W}{L}_3}} + \left(V_{Tn} + \sqrt{\frac{2I_{D1}}{\mu C_{ox} \frac{W}{L}_1}} \right)$$

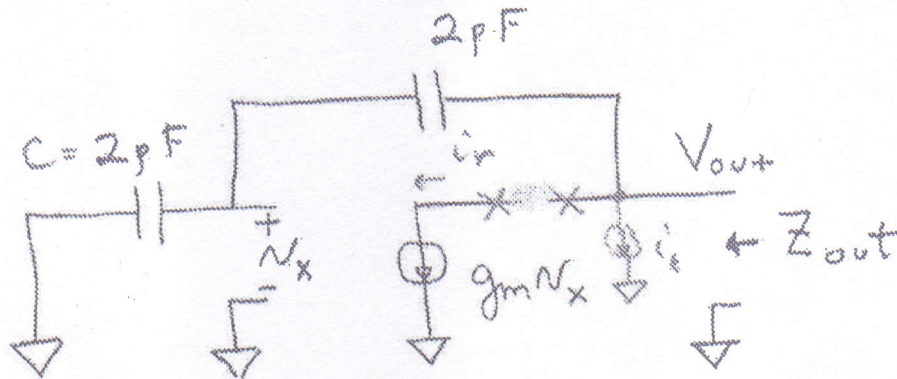
$$= -2.5V + 1.49V + (1V + 0.11)V$$

$$= \underline{\underline{0.1V}}$$

④

5. a) Find the frequency at which the magnitude of the return ratio equals 1 for the circuit below.

ω_u' = Frequency where $|RR| = 1$, g_m/C ; $C = 2pF$



$$\left. \begin{aligned} N_x &= -\frac{1}{j\omega C} i_t \\ i_r &= g_m N_x \end{aligned} \right\} i_r = -\frac{g_m}{j\omega C} i_t$$

$$RR = -\frac{i_r}{i_t} = \frac{g_m}{j\omega C}$$

$$|RR| = 1 = \frac{g_m}{\omega C}$$

$$\omega = \frac{g_m}{C}$$

$$C = 2pF$$

5 (continued)

b) Use Blackman's impedance formula to compute the magnitude of the output impedance at the frequency computed in part (a).

$$|Z_{out}| = \frac{\sqrt{2}}{g_m}$$

$$\omega | g_m = 0 : Z_{out} \leftrightarrow 1 \mu F = (2 \mu F || 2 \mu F)$$

$$R.R(\text{out shorted}) = 0$$

$$R.R(\text{out open}) = \frac{g_m}{j\omega C} = \frac{1}{j} = -j @ \omega_u'$$

$$Z_{out}(\omega_u') = \frac{\frac{1}{j\omega_u'(1 \mu F)} (1 + 0)}{1 - j}$$

$$|Z_{out}(\omega_u')| = \frac{1}{\omega_u'(1 \mu F)} \left| \frac{1}{1 - j} \right|$$

$$= \frac{1}{\frac{g_m}{C} (1 \mu F)} \cdot \frac{1}{\sqrt{2}} =$$

$$= \frac{2}{g_m} \cdot \frac{1}{\sqrt{2}} = \frac{\sqrt{2}}{g_m}$$

$$C = 2 \mu F$$