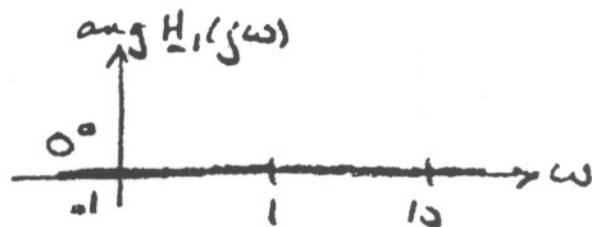
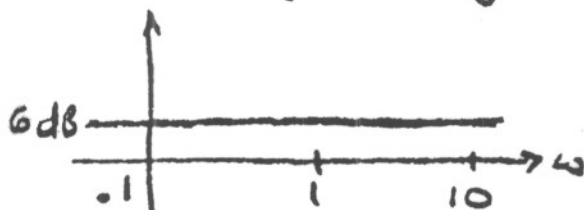
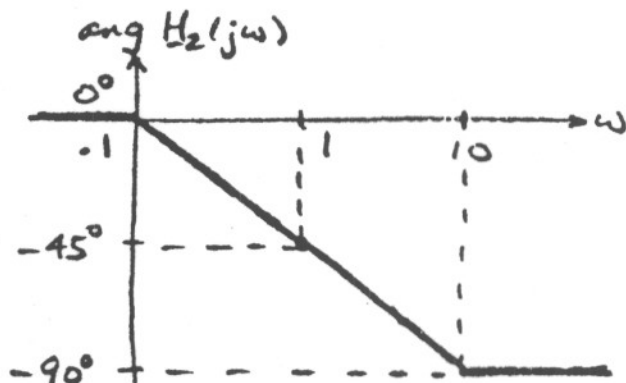
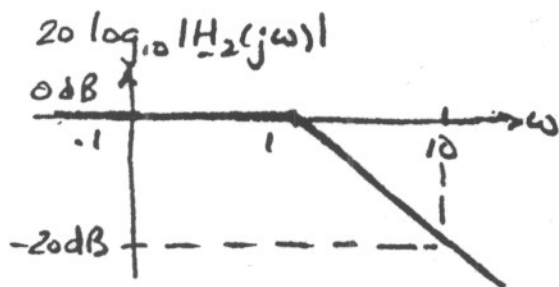


5.19 $H_1(j\omega) = 2 \Rightarrow |H_1(j\omega)| = 2 \quad \text{ang } H_1(j\omega) = 0^\circ$

$20 \log_{10} |H_1(j\omega)| = 20 \log_{10} 2 = 6 \text{ dB}$

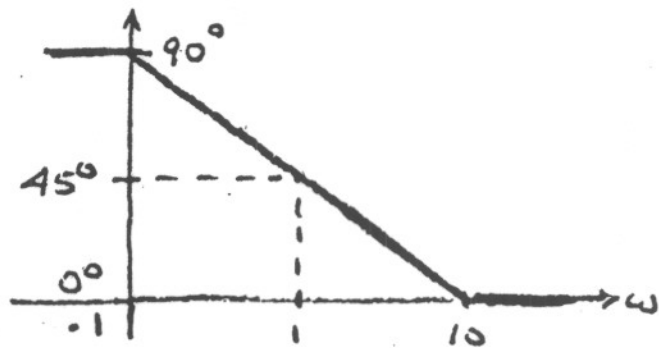
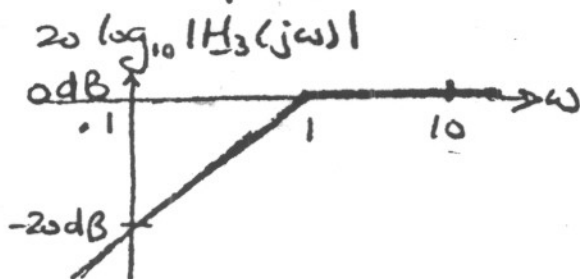


$H_2(j\omega) = \frac{1}{1+j\omega} \Rightarrow |H_2(j\omega)| = \frac{1}{\sqrt{1+\omega^2}} \quad \text{ang } H_2(j\omega) = -\tan^{-1}\omega$

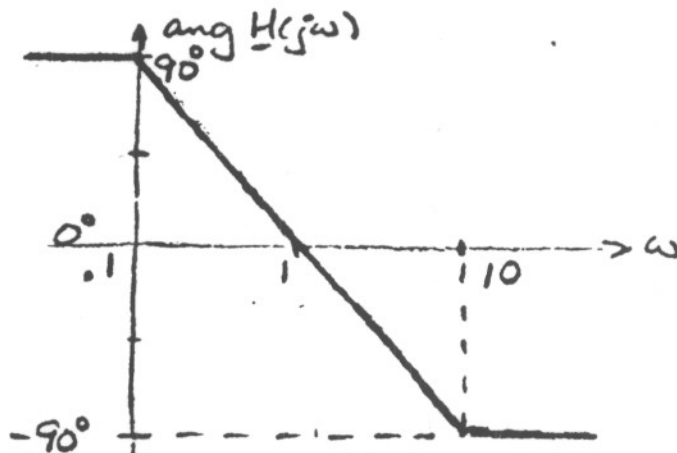
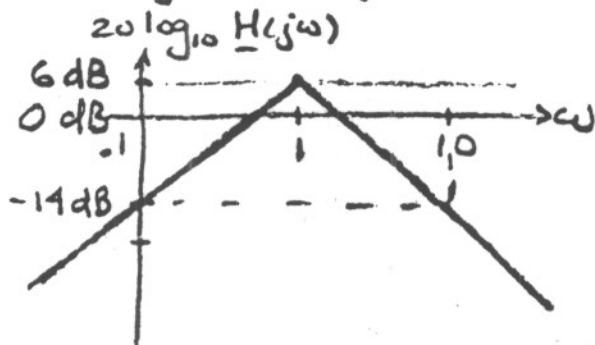


$H_3(j\omega) = \frac{j\omega}{1+j\omega}$

$|H_3(j\omega)| = \frac{\omega}{\sqrt{1+\omega^2}} \quad \text{ang } H_3(j\omega) = 90^\circ - \tan^{-1}\omega$

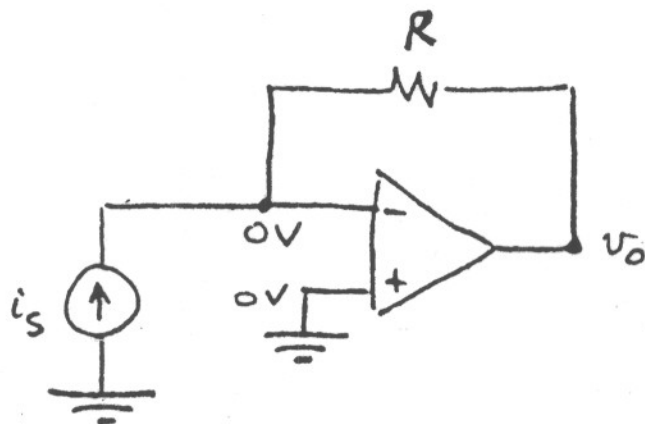


Adding the plots yields



This is a band pass filter.

2.27 (a)

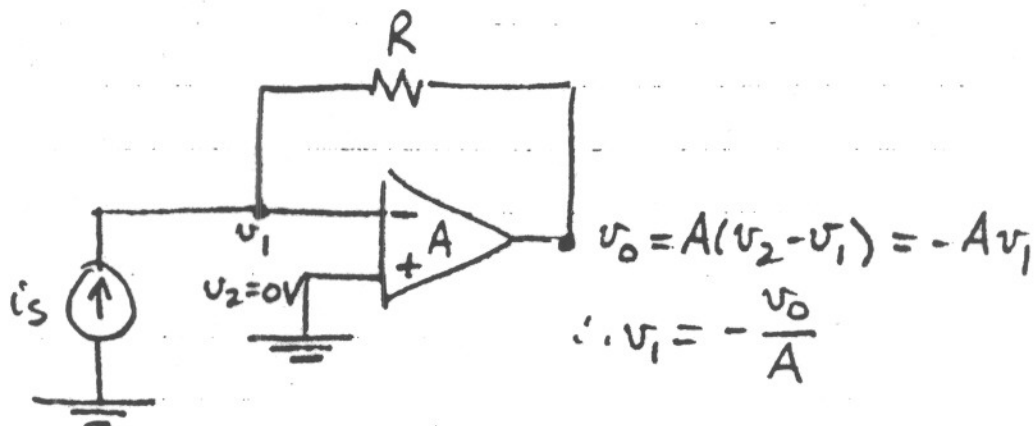


By KCL at the inverting input of the op amp,

$$i_s + \frac{v_o}{R} = 0$$

$$i_s = -\frac{v_o}{R} \Rightarrow \underline{\underline{v_o = -Ri_s}}$$

(b)

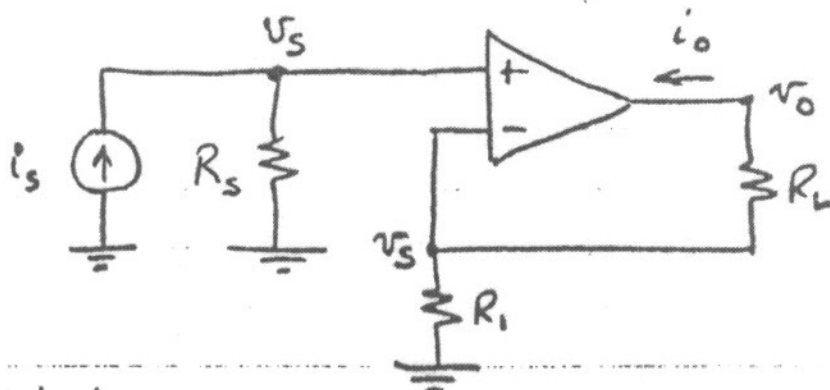


By KCL at node v_1 ,

$$i_s = \frac{v_1 - v_o}{R} = \frac{-\frac{v_o}{A} - v_o}{R} = -\frac{v_o + Av_o}{AR} = -\frac{1+A}{AR} v_o$$

$$\therefore \underline{\underline{v_o = -\frac{AR}{1+A} i_s}}$$

2.29



(a)

By Ohm's law,

$$v_s = R_s i_s$$

By KCL at the inverting input of the op amp,

$$\frac{v_s}{R_1} + \frac{v_s - v_o}{R_L} = 0$$

$$R_L v_s + R_1 v_s - R_1 v_o = 0$$

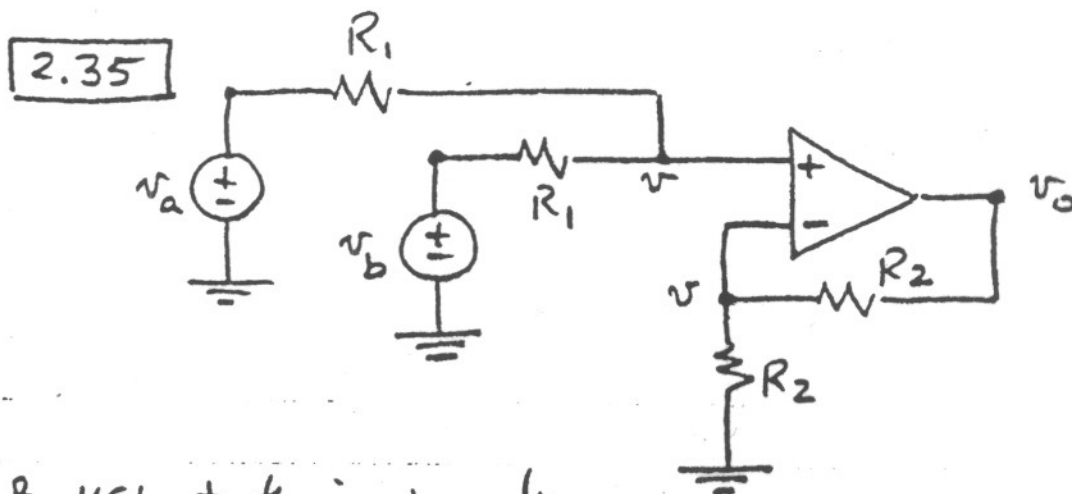
$$(R_1 + R_L) v_s = R_1 v_o$$

$$v_o = \frac{(R_1 + R_L) v_s}{R_1} = \frac{(R_1 + R_L) R_s i_s}{R_1} = \underline{\underline{\left(\frac{R_L}{R_1} + 1\right) R_s i_s}}$$

(b)

By Ohm's law,

$$i_o = -\frac{v_s}{R_1} = -\frac{R_s i_s}{R_1} = \underline{\underline{-\frac{R_s}{R_1} i_s}}$$



By KCL at the noninverting input of the op amp,

$$\frac{v - v_a}{R_1} + \frac{v - v_b}{R_1} = 0$$

$$v - v_a + v - v_b = 0$$

$$2v = v_a + v_b$$

$$\therefore \underline{\underline{v_o = v_a + v_b}}$$

By KCL at the inverting input of the op amp,

$$\frac{v}{R_2} + \frac{v - v_o}{R_2} = 0$$

$$v + v - v_o = 0$$

$$2v = v_o$$