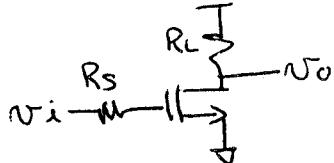


(1)

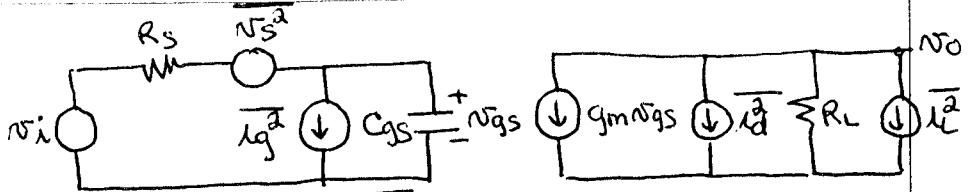


$$\frac{N_{o1}^2}{1} = 4kT R_S \Delta f$$

$$\frac{1g^2}{1} = 2g I_G \Delta f \approx 0$$

$$\frac{1L^2}{1} = \frac{4kT}{R_L} \Delta f$$

$$\frac{1d^2}{1} = 4kT \frac{2}{3} q_m \Delta f + \frac{q_m^2 K_f \Delta f}{w L C_{ox} F}$$



$$q_m = \sqrt{2(194)(100)(100)} = 1.97 \text{ mA/V}$$

$$C_{ox} = \frac{3.4 \times 8.854 \times 10^{-14}}{80 \times 10^{-8}} = 4.3 \times 10^{-7} \frac{\text{F}}{\text{cm}^2} = 4.3 \text{ fF}/\mu\text{m}^2$$

$$\text{Let } A_N(\omega) = \frac{V_O}{V_I} (\omega)$$

$$A_N(\omega) = -\frac{q_m R_L}{1 + g_m R_S}$$

$$C_{gs} = \frac{2}{3}(100)(4.3 \text{ fF}) = 287 \text{ fF}$$

$$f_{-3dB} = \frac{1}{2\pi C_{gs} R_S} = 5.55 \text{ MHz}$$

Output noise due to  $\frac{N_{o1}^2}{1} = \frac{N_{o1}^2}{1} = A_N^2(\omega) \frac{N_S^2}{1}$

Output noise due to  $\frac{1d^2}{1} = \frac{N_{o2}^2}{1} = \frac{1d^2}{1} R_L^2$

Output noise due to  $\frac{1L^2}{1} = \frac{N_{o3}^2}{1} = \frac{1L^2}{1} R_L^2$

At 10 Hz,  $|A_N| = 19.7$

$$\frac{N_{o1}^2}{1} = \frac{(19.7)^2 (1.66 \times 10^{-20})(10^5) \Delta f}{100(1)(4.3 \times 10^{-15}) 10} = 6.44 \times 10^{-13} \Delta f (\text{V}^2)$$

$$\frac{N_{o2}^2}{1} = \frac{(1.66 \times 10^{-20}) \frac{2}{3} (1.97 \times 10^{-3})(10^4)^2 \Delta f + (1.97 \times 10^{-3})^2 (3 \times 10^{-24}) \Delta f (10^4)^2}{100(1)(4.3 \times 10^{-15}) 10}$$

$$= [2.18 \times 10^{-15} \Delta f + 2.71 \times 10^{-10} \Delta f] (\text{V}^2)$$

$$\frac{N_{o3}^2}{1} = \frac{1.66 \times 10^{-20} (10^4) \Delta f}{100(1)(4.3 \times 10^{-15}) 10} = 1.66 \times 10^{-16} \Delta f (\text{V}^2)$$

$$\frac{N_{o1}^2}{1} + \frac{N_{o2}^2}{1} + \frac{N_{o3}^2}{1} = 2.72 \times 10^{-10} \Delta f (\text{V}^2)$$

$$\frac{N_{ot}^2}{1} = 16.5 \text{ nV} \sqrt{\Delta f} \quad (\text{SPICE: } 16.4 \text{ nV} \sqrt{\Delta f})$$

$$\text{Total input-referred noise} = \sqrt{\frac{N_{ot}^2}{1}} = \sqrt{\frac{N_{ot}^2}{1} / |A_N|} = 837 \text{ nV} \sqrt{\Delta f}$$

$$\text{SPICE: } 835 \text{ nV} \sqrt{\Delta f}$$

At 100 kHz,  $|A_N| \approx 19.7$

$$\frac{N_{o1}^2}{1} = \text{same}$$

$$\frac{N_{o2}^2}{1} = (2.18 \times 10^{-15} \Delta f + 2.71 \times 10^{-14} \Delta f) (\text{V}^2)$$

$$\frac{N_{o3}^2}{1} = \text{same}$$

$$\frac{N_{o1}^2}{1} = 6.73 \times 10^{-13} \Delta f (\text{V}^2)$$

$$\frac{N_{ot}^2}{1} = 821 \text{ nV} \sqrt{\Delta f} \quad (\text{SPICE: } 817 \text{ nV} \sqrt{\Delta f})$$

$$\frac{N_{ot}^2}{1} = 41.7 \text{ nV} \sqrt{\Delta f} \quad (\text{SPICE: } 41.5 \text{ nV} \sqrt{\Delta f})$$

At 1 GHz,  $|A_N| = 19.7 / \sqrt{1 + (1000/5.55)^2} = 0.109$

$$\frac{N_{o1}^2}{1} = (0.109)^2 (1.66 \times 10^{-20})(10^5) \Delta f = 1.98 \times 10^{-17} \Delta f (\text{V}^2)$$

$$\frac{N_{o2}^2}{1} = 2.18 \times 10^{-15} \Delta f + 2.71 \times 10^{-18} \Delta f$$

$$\frac{N_{o3}^2}{1} = \text{same}$$

$$\frac{N_{ot}^2}{1} = 2.37 \times 10^{-15}$$

$$\frac{N_{ot}^2}{1} = 48.7 \text{ nV} \sqrt{\Delta f} \quad (\text{SPICE: } 48.5 \text{ nV} \sqrt{\Delta f})$$

$$\frac{N_{ot}^2}{1} = 48.7 \text{ nV} \sqrt{\Delta f} / 0.109 = 446 \text{ nV} \sqrt{\Delta f} \quad (\text{SPICE: } 445 \text{ nV} \sqrt{\Delta f})$$

Therefore,

At 10 Hz, 1/f noise dominates

At 100 Hz, thermal noise from  $R_S$  dominates

At 1 GHz, thermal noise from the transistor dominates

$$K_D' = \mu_D C_{OX} = 150 (4.3 \times 10^{-7}) = 64.7 \mu A/V^2$$

$$K_N' = \mu_N C_{OX} = 450 (4.3 \times 10^{-7}) = 194 \mu A/V^2$$

$$q_{m_1} = \sqrt{2(64.7)(150)(0.72)(100)} = 1.64 \text{ mA/V}$$

$$q_{m_3} = \sqrt{2(194)(50)(0.72)(100)} = 1.64 \text{ mA/V} = q_{m_1}$$

Noise is dominated by M<sub>1</sub>-M<sub>4</sub>

At 100Hz

$$M_{1,2} \text{ thermal: } \frac{2}{3} \frac{4KT}{q_{m_1}} \Delta f = \frac{2}{3} \frac{(1.66 \times 10^{-20})}{1.64 \text{ m}} = 6.75 \times 10^{-18} \Delta f \text{ (V}^2\text{)}$$

$$M_{1,2} \text{ flicker: } \frac{K_f \Delta f}{WL C_{OX} f} = \frac{3 \times 10^{-24} \Delta f}{150(0.72)(4.3 \times 10^{-15})100} = 6.46 \times 10^{-14} \Delta f \text{ (V}^2\text{)}$$

$$M_{3,4} \text{ thermal: } \frac{2}{3} \frac{4KT}{q_{m_3}} \frac{q_{m_3}^2}{q_{m_1}^2} \Delta f = \frac{2}{3} \frac{(1.66 \times 10^{-20})}{1.64 \text{ m}} = 6.75 \times 10^{-18} \Delta f \text{ (V}^2\text{)}$$

$$M_{3,4} \text{ flicker: } \frac{K_f \Delta f}{WL C_{OX} f} \frac{q_{m_3}^2}{q_{m_1}^2} = \frac{3 \times 10^{-24} \Delta f}{50(0.72)(4.3 \times 10^{-15})100} = 1.94 \times 10^{-13} \Delta f \text{ (V}^2\text{)}$$

$$\overline{N_{AT}^2} = 2 [6.75 \times 10^{-18} + 6.46 \times 10^{-14} + 6.75 \times 10^{-18} + 1.94 \times 10^{-13}] \Delta f$$

$$\sqrt{\overline{N_{AT}^2}} = 5.17 \times 10^{-13} \Delta f \text{ (V}^2\text{)}$$

$$\sqrt{\overline{N_{AT}^2}} = 71.9 \text{ nV} \sqrt{\Delta f} \quad (\text{SPICE: } 699 \text{ nV} \sqrt{\Delta f})$$

Flicker noise is dominant, especially from M<sub>3</sub>+M<sub>4</sub>

At 1kHz

M<sub>1,2</sub> thermal = same

$$M_{1,2} \text{ flicker} = 6.46 \times 10^{-15} \Delta f \text{ (V}^2\text{)}$$

M<sub>3,4</sub> thermal = same

$$M_{3,4} \text{ flicker} = 1.94 \times 10^{-14} \Delta f \text{ (V}^2\text{)}$$

$$\overline{N_{AT}^2} = 5.17 \times 10^{-14} \Delta f \text{ (V}^2\text{)}$$

$$\sqrt{\overline{N_{AT}^2}} = 22.7 \text{ nV} \sqrt{\Delta f} \quad (\text{SPICE: } 221 \text{ nV} \sqrt{\Delta f})$$

At 10kHz

M<sub>1,2</sub> thermal = same

$$M_{1,2} \text{ flicker} = 6.46 \times 10^{-16} \Delta f \text{ (V}^2\text{)}$$

M<sub>3,4</sub> thermal = same

$$M_{3,4} \text{ flicker} = 1.94 \times 10^{-15} \Delta f \text{ (V}^2\text{)}$$

$$\overline{N_{AT}^2} = 5.20 \times 10^{-15} \Delta f \text{ (V}^2\text{)}$$

$$\sqrt{\overline{N_{AT}^2}} = 72.1 \text{ nV} \sqrt{\Delta f} \quad (\text{SPICE: } 70.0 \text{ nV} \sqrt{\Delta f})$$