

## Reliable Decentralized Control

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### Abstract

We study reliable stabilization of linear, time-invariant, multi-input multi-output, two-channel decentralized control systems. We develop necessary and sufficient conditions for reliable decentralized stabilizability under sensor or actuator failures and present reliable decentralized controller design methods for strongly stabilizable plants.

### 1. Introduction

We consider the reliable stabilization problem using the linear, time-invariant (LTI), multi-input, multi-output (MIMO), two-channel decentralized system configuration  $\mathcal{S}(P, C_d)$  (Figure 1). The reliable stabilization problem aims to find two controllers such that the system  $\mathcal{S}(P, C_d)$  is stable when both controllers are acting together (normal mode) and when each controller is acting alone (failure mode). The failure of a controller is modeled by setting its transfer-function equal to zero.

A multi-controller system configuration achieving reliable stabilization was introduced in [5], [6]. Factorization methods were used in [2], [3], [9] to study reliable stability with two full-feedback controllers; it was shown that a given plant can be reliably stabilized with two full-feedback controllers if and only if it is strongly stabilizable (i.e., it can be stabilized using a stable controller) in the standard unity-feedback system. Reliable stabilization using a two-channel decentralized control system was considered in [7].

In this paper, we develop necessary and sufficient conditions for existence of decentralized controllers, which achieve reliable stability. For certain classes of plants we present decentralized controller design methods. Due to the algebraic methods used

\*Research supported by the National Science Foundation Grant ECS-9257932.

here, the results apply to continuous-time as well as discrete-time systems.

### 2. Main Results

**Notation:** • Let  $\mathcal{M}(\mathcal{R})$  be the set of matrices whose entries are in  $\mathcal{R} \subset \mathcal{R}_p$ , where  $\mathcal{R}_p$  denotes proper rational functions with real coefficients and  $\mathcal{R}$  denotes proper rational functions which do not have any poles in the region of instability  $\mathcal{U}$ ; here  $\mathcal{U}$  contains the extended closed right-half-plane (for continuous-time systems) or the complement of the open unit-disk (for discrete-time systems). A map  $M$  is called  $\mathcal{R}$ -stable iff  $M \in \mathcal{M}(\mathcal{R})$ ; An  $\mathcal{R}$ -stable map  $M$  is  $\mathcal{R}$ -unimodular iff  $M^{-1}$  is also  $\mathcal{R}$ -stable. • Let the norm of an  $\mathcal{R}$ -stable map  $M \in \mathcal{M}(\mathcal{R})$  be defined as  $\|M\| = \sup_{s \in \partial\mathcal{U}} \bar{\sigma}(M(s))$ , where  $\bar{\sigma}$  denotes the maximum singular value and  $\partial\mathcal{U}$  denotes the boundary of  $\mathcal{U}$ . • A right-coprime-factorization (RCF) and a left-coprime-factorization (LCF) of  $P \in \mathcal{R}_p^{n_o \times n_i}$  are denoted by  $(N_P, D_P)$  and  $(\tilde{D}_P, \tilde{N}_P)$ , where  $N_P, D_P, \tilde{N}_P, \tilde{D}_P \in \mathcal{M}(\mathcal{R})$ ,  $D_P$  and  $\tilde{D}_P$  are biproper and  $P = N_P D_P^{-1} = \tilde{D}_P^{-1} \tilde{N}_P$ .

#### 2.1. System description

Consider the LTI, MIMO, two-channel decentralized control system  $\mathcal{S}(P, C_d)$  shown in Figure 1:  $\mathcal{S}(P, C_d)$  is a well-posed system, where

$$P = \begin{bmatrix} P_{11} & P_{12} \\ P_{21} & P_{22} \end{bmatrix} \in \mathcal{R}_p^{n_o \times n_i},$$

$$C_d = \text{diag} [C_1, C_2] \in \mathcal{R}_p^{n_i \times n_o},$$

$C_j \in \mathcal{R}_p^{n_{ij} \times n_{oj}}$ ,  $j = 1, 2$ ;  $P$  and  $C_d$  represent the plant and the decentralized controller, respectively. It is assumed that  $P$  and  $C_d$  do not have any hidden modes associated with eigenvalues in  $\mathcal{U}$ . For  $j = 1, 2$ ,  $F_{Sj}$  and  $F_{Aj}$  are  $\mathcal{R}$ -stable maps representing sensor and actuator failures in the first and second

channels, respectively. Under normal operation,  $F_{Sj} = I$  and  $F_{Aj} = I$ ; the (complete disconnection) failure of the  $j$ -th channel is represented by setting the corresponding  $F_{Sj}$  or  $F_{Aj}$  equal to zero.

Using an RCF  $(N_P, D_P)$  of  $P$  and an LCF  $(\tilde{D}_{Cj}, \tilde{N}_{Cj})$  of  $C_j$ , with  $D_P \xi_P = e_P$  and  $\tilde{D}_{Cj} y_{Cj} = \tilde{N}_{Cj} e_{Cj}$ ,  $j = 1, 2$ ,  $\tilde{D}_C = \text{diag}[\tilde{D}_{C1}, \tilde{D}_{C2}]$ ,  $\tilde{N}_C = \text{diag}[\tilde{N}_{C1}, \tilde{N}_{C2}]$ ,  $F_S = \text{diag}[F_{S1}, F_{S2}]$ ,  $F_A = \text{diag}[F_{A1}, F_{A2}]$ ,  $u_P = (u_{P1}, u_{P2})$ ,  $u_C = (u_{C1}, u_{C2})$ ,  $y_P = (y_{P1}, y_{P2})$ ,  $y_C = (y_{C1}, y_{C2})$ , the system  $\mathcal{S}(P, C_d)$  is described as follows:

$$\begin{bmatrix} D_P & -F_A \\ \tilde{N}_C F_S N_P & \tilde{D}_C \end{bmatrix} \begin{bmatrix} \xi_P \\ y_C \end{bmatrix} = \begin{bmatrix} I & 0 \\ 0 & \tilde{N}_C \end{bmatrix} \begin{bmatrix} u_P \\ u_C \end{bmatrix},$$

$$\begin{bmatrix} y_P \\ y_C \end{bmatrix} = \begin{bmatrix} N_P & 0 \\ 0 & I \end{bmatrix} \begin{bmatrix} \xi_P \\ y_C \end{bmatrix}. \quad (1)$$

Equation (1) is of the form  $D_H \xi = u$ ,  $y = N \xi$ . The system  $\mathcal{S}(P, C_d)$  is well-posed if and only if the map  $D_H$  is biproper, equivalently, the closed-loop map  $H : (u_P, u_C) \mapsto (y_P, y_C)$  is proper;  $\mathcal{S}(P, C_d)$  is automatically well-posed if  $P$  or  $C_d$  is strictly proper.

## 2.2. Conditions for stability

Following standard definitions, with  $F_S$  and  $F_A$   $\mathcal{R}$ -stable, the system  $\mathcal{S}(P, C_d)$  is  $\mathcal{R}$ -stable iff the closed-loop map  $H$  from  $(u_P, u_C)$  to  $(y_P, y_C)$  is  $\mathcal{R}$ -stable. From the system description (1),  $\mathcal{S}(P, C_d)$  is  $\mathcal{R}$ -stable if and only if the map  $D_H$  is  $\mathcal{R}$ -unimodular. The decentralized controller  $C_d$  is called an  $\mathcal{R}$ -stabilizing controller for  $P$  iff  $C_d$  is proper and  $\mathcal{S}(P, C_d)$  is  $\mathcal{R}$ -stable.

We now investigate  $\mathcal{R}$ -stability of the system  $\mathcal{S}(P, C_d)$  under various failure cases. Without loss of generality, we assume that the RCF  $(N_P, D_P)$  and the LCF  $(\tilde{D}_P, \tilde{N}_P)$  of  $P$  have a lower-triangular denominator matrix  $D_P$  and an upper-triangular denominator matrix  $\tilde{D}_P$  [1]; i.e.,

$$\begin{aligned} P &= N_P D_P^{-1} = \begin{bmatrix} N_{11} & N_{12} \\ N_{21} & N_{22} \end{bmatrix} \begin{bmatrix} D_{11} & 0 \\ D_{21} & D_{22} \end{bmatrix}^{-1} \\ &= \tilde{D}_P^{-1} \tilde{N}_P = \begin{bmatrix} \tilde{D}_{11} & \tilde{D}_{12} \\ 0 & \tilde{D}_{22} \end{bmatrix}^{-1} \begin{bmatrix} \tilde{N}_{11} & \tilde{N}_{12} \\ \tilde{N}_{21} & \tilde{N}_{22} \end{bmatrix}. \end{aligned} \quad (2)$$

Then from (1), the nominal system  $\mathcal{S}(P, C_d)$  without failure is  $\mathcal{R}$ -stable if and only if  $D_H$  is  $\mathcal{R}$ -unimodular,

equivalently,

$$\begin{bmatrix} \tilde{D}_{C1} D_{11} + \tilde{N}_{C1} N_{11} & \tilde{N}_{C1} N_{12} \\ \tilde{D}_{C2} D_{21} + \tilde{N}_{C2} N_{21} & \tilde{D}_{C2} D_{22} + \tilde{N}_{C2} N_{22} \end{bmatrix}$$

is  $\mathcal{R}$ -unimodular. (3)

*Case 1: Sensor failure in the first channel:* Suppose that  $F_{A1} = I$ ,  $F_{A2} = I$  and  $F_{S2} = I$ . Then  $\mathcal{S}(P, C_d)$  is  $\mathcal{R}$ -stable with  $F_{S1} = 0$  if and only if

$$D_{11} = I, \quad \tilde{D}_{C2} D_{22} + \tilde{N}_{C2} N_{22} = I \quad (4)$$

and

$$\tilde{D}_{C1} = I. \quad (5)$$

Therefore, there exists an  $\mathcal{R}$ -stabilizing decentralized controller  $C_d$  for the plant  $P$  if and only if  $P$  is of the form

$$P = N_P D_P^{-1} = \begin{bmatrix} N_{11} & N_{12} \\ \tilde{V}_{22} \tilde{N}_{21} & N_{22} \end{bmatrix} \begin{bmatrix} I & 0 \\ -\tilde{U}_{22} \tilde{N}_{21} & D_{22} \end{bmatrix}^{-1},$$

$(N_{22}, D_{22})$  right-coprime (6)

and  $\tilde{U}_{22}$ ,  $\tilde{V}_{22}$  are  $\mathcal{R}$ -stable matrices satisfying the following identity for the RCF  $N_{22} D_{22}^{-1}$  of  $P_{22}$  for some  $\mathcal{R}$ -stable matrices  $U_{22}$ ,  $V_{22}$  [1]:

$$\begin{bmatrix} V_{22} & U_{22} \\ -\tilde{N}_{22} & \tilde{D}_{22} \end{bmatrix} \begin{bmatrix} D_{22} & -\tilde{U}_{22} \\ N_{22} & \tilde{V}_{22} \end{bmatrix} = I. \quad (7)$$

By (4),  $C_d \in \mathcal{M}(\mathcal{R}_p)$  is a decentralized  $\mathcal{R}$ -stabilizing controller for  $P$  if and only if  $C_1$  is  $\mathcal{R}$ -stable and  $C_2$  is an  $\mathcal{R}$ -stabilizing controller for  $P_{22}$ , i.e.,

$$C_d = \text{diag}[C_1, C_2], \quad C_1 \in \mathcal{R}^{n_{o1} \times n_{i1}},$$

$$\begin{aligned} C_2 &= (V_{22} - Q_2 \tilde{N}_{22})^{-1} (U_{22} + Q_2 \tilde{D}_{22}) \\ &= (\tilde{U}_{22} + D_{22} Q_2) (\tilde{V}_{22} + N_{22} Q_2)^{-1} \end{aligned} \quad (8)$$

for some  $\mathcal{R}$ -stable  $Q_2$  such that

$$(V_{22} - Q_2 \tilde{N}_{22}) \text{ is biproper; } \quad (9)$$

note that (9) automatically holds for all  $Q_2 \in \mathcal{M}(\mathcal{R})$  when  $P_{22}$  is strictly proper [8].

Now  $\mathcal{S}(P, C_d)$  is  $\mathcal{R}$ -stable with the controller  $C_d$  in (8) assuming that  $F_{S1} = 0$ ; but the controller should be designed to ensure  $\mathcal{R}$ -stability for the nominal system as well. From (2), (6) and (8),  $D_{21} = -\tilde{U}_{22} \tilde{N}_{21}$ ,  $N_{21} = \tilde{V}_{22} \tilde{N}_{21}$  and  $(\tilde{D}_{C2} D_{21} + \tilde{N}_{C2} N_{21}) = Q_2 \tilde{N}_{21}$  [1]. The decentralized controller  $C_d$  is an  $\mathcal{R}$ -stabilizing controller for  $P$  for both

of the possibilities of  $F_{S1} = I$  and  $F_{S1} = 0$  if and only if  $C_2$  is the same as in (8) but  $C_1$  is given by

$$C_1 = (I - Q_1(N_{11} - N_{12}Q_2\tilde{N}_{21}))^{-1}Q_1, \quad (10)$$

where the  $Q_1 \in \mathcal{R}^{n_1 \times n_1}$  is such that

$$\tilde{D}_{C1} = I - Q_1(N_{11} - N_{12}Q_2\tilde{N}_{21}) \quad (11)$$

is  $\mathcal{R}$ -unimodular.

*Case 2: Actuator failure in the first channel:* Suppose that  $F_{S1} = I$ ,  $F_{S2} = I$  and  $F_{A2} = I$ . Then  $\mathcal{S}(P, C_d)$  is  $\mathcal{R}$ -stable with  $F_{A1} = 0$  if and only if (4)-(5) hold, i.e., if and only if  $\mathcal{S}(P, C_d)$  is  $\mathcal{R}$ -stable with  $F_{S1} = 0$ . Therefore, there exists an  $\mathcal{R}$ -stabilizing decentralized controller  $C_d$  for the plant  $P$  if and only if  $P$  is of the form in (6) and  $C_d \in \mathcal{M}(\mathcal{R}_p)$  is a decentralized  $\mathcal{R}$ -stabilizing controller for  $P$  if and only if it is of the form given by (8). As in the sensor failure case above, the decentralized controller  $C_d$  is an  $\mathcal{R}$ -stabilizing controller for  $P$  for both of the possibilities of  $F_{A1} = I$  and  $F_{A1} = 0$  if and only if  $C_2$  is the same as in (8) but  $C_1$  is given by (10), where  $Q_1$  is such that (11) is  $\mathcal{R}$ -unimodular.

*Case 3: Simultaneous sensor and actuator failure in the first channel:* Suppose that  $F_{S2} = I$  and  $F_{A2} = I$ . Then  $\mathcal{S}(P, C_d)$  is  $\mathcal{R}$ -stable with  $F_{S1} = 0$  and  $F_{A1} = 0$  if and only if (4) holds. In this case (5) is not needed because when both the sensors and actuators of the first channel fail,  $y_{C1} = 0$ ; since  $C_1$  is no longer taken into account, it need not be  $\mathcal{R}$ -stable. Therefore, there exists an  $\mathcal{R}$ -stabilizing decentralized controller  $C_d$  for the plant  $P$  if and only if  $P$  is of the form in (2) and  $C_d \in \mathcal{M}(\mathcal{R}_p)$  is a decentralized  $\mathcal{R}$ -stabilizing controller for  $P$  if and only if  $C_2$  is of the form given by (8). Now the same controller will also  $\mathcal{R}$ -stabilize the nominal system  $\mathcal{S}(P, C_d)$  without failure if and only if the additional constraint (10) is put on  $C_1$ , except that the  $\mathcal{R}$ -stable matrix  $Q_1$  is chosen such that the matrix in (11) biproper since  $C_1$  need not be  $\mathcal{R}$ -stable in this case; note that (11) is biproper for any strictly proper  $Q_1$ .

*Case 4: Sensor failure in the second channel:* Suppose that  $F_{A1} = I$ ,  $F_{A2} = I$  and  $F_{S1} = I$ . Then  $\mathcal{S}(P, C_d)$  is  $\mathcal{R}$ -stable with  $F_{S2} = 0$  if and only if

$$\begin{bmatrix} \tilde{D}_{C1} D_{11} + \tilde{N}_{C1} N_{11} & \tilde{N}_{C1} N_{12} \\ D_{21} & D_{22} \end{bmatrix} \text{ is } \mathcal{R}\text{-unimodular} \quad (12)$$

and

$$\tilde{D}_{C2} = I. \quad (13)$$

Therefore,  $C_2$  is necessarily  $\mathcal{R}$ -stable.

Now the system  $\mathcal{S}(P, C_d)$  is  $\mathcal{R}$ -stable for either  $F_{S2} = I$  or  $F_{S2} = 0$  (i.e., with or without sensor failure of the second channel) if and only if both (3) and (12) hold.

*Case 5: Actuator failure in the second channel:* Suppose that  $F_{S1} = I$ ,  $F_{S2} = I$  and  $F_{A1} = I$ . Then  $\mathcal{S}(P, C_d)$  is  $\mathcal{R}$ -stable with  $F_{A2} = 0$  if and only if (12) holds, i.e., if and only if  $\mathcal{S}(P, C_d)$  is  $\mathcal{R}$ -stable with  $F_{S2} = 0$ . As in the sensor failure case above,  $\mathcal{S}(P, C_d)$  is  $\mathcal{R}$ -stable for either  $F_{A2} = I$  or  $F_{A2} = 0$  (i.e., with or without actuator failure of the second channel) if and only if both (3) and (12) hold.

*Case 6: Simultaneous sensor and actuator failure in the second channel:* Suppose that  $F_{S1} = I$  and  $F_{A1} = I$ . Then  $\mathcal{S}(P, C_d)$  is  $\mathcal{R}$ -stable with  $F_{S2} = 0$  and  $F_{A2} = 0$  if and only if (12) holds. In this case, (13) is not needed because when both sensors and actuators of the second channel fail,  $y_{C2} = 0$ ; since  $C_2$  is no longer taken into account, it need not be  $\mathcal{R}$ -stable. Now the nominal system  $\mathcal{S}(P, C_d)$  is also  $\mathcal{R}$ -stable if and only if (3) also holds in addition to condition (12).

*Case 7: Simultaneous sensor and actuator failure in either the first or the second channel:* We now investigate  $\mathcal{R}$ -stability of the system  $\mathcal{S}(P, C_d)$  under simultaneous sensor and actuator failure in either the first or the second channel; this is the same as the reliable decentralized stabilization problem studied in [7]. We study this case in detail in section 2.3 below.

### 2.3. Reliable decentralized stabilizability

The system  $\mathcal{S}(P, C_d)$  is said to be reliably stabilized iff  $\mathcal{S}(P, C_d)$  is  $\mathcal{R}$ -stable under any of the following three conditions:

- i) The nominal system  $\mathcal{S}(P, C_d)$  is stable, i.e.,  $F_S = I$  and  $F_A = I$
- ii) the system  $\mathcal{S}(P, C_d)$  is stable with simultaneous sensor and actuator failure in the first channel, i.e.,  $F_{S1} = 0$ ,  $F_{A1} = 0$ ,  $F_{S2} = I$ ,  $F_{A2} = I$
- iii) the system  $\mathcal{S}(P, C_d)$  is stable with simultaneous sensor and actuator failure in the second channel, i.e.,  $F_{S2} = 0$ ,  $F_{A2} = 0$ ,  $F_{S1} = I$ ,  $F_{A1} = I$ .

Now the first of these conditions is satisfied if and only if (3) holds. The second condition was explained in case 3 of section 2.2 above; it is satisfied if and only

if (4) holds. The third condition was explained in case 6 of section 2.2 above; it is satisfied if and only if (12) holds. Note that  $P$  is of the form given by (6) for conditions 2 and 3 to hold. Putting (3), (4) and (12) together with the necessary form of  $P$  in (6), we conclude that the system  $\mathcal{S}(F_S, P, F_A, C)$  is reliably stabilized if and only if

$$D_{22} - N_{C2} \tilde{N}_{21} Q_1 N_{12} \text{ is } \mathcal{R}\text{-unimodular.} \quad (14)$$

Furthermore,  $C_d = \text{diag}[C_1, C_2]$  is a decentralized  $\mathcal{R}$ -stabilizing controller such that  $\mathcal{S}(P, C_d)$  is reliably stabilized if and only if  $C_1$  and  $C_2$  are given by (10) and (8), respectively, for some  $\mathcal{R}$ -stable  $Q_1$  and  $Q_2$  (of appropriate sizes) satisfying (11) and (9) and are such that (14) holds, i.e.,

$$D_{22} + (\tilde{U}_{22} + D_{22} Q_2) \tilde{N}_{21} Q_1 N_{12} \text{ is } \mathcal{R}\text{-unimodular.} \quad (15)$$

Although condition (15) characterizes all parameter matrices  $Q_1$  and  $Q_2$  that achieve reliable stabilization of  $\mathcal{S}(P, C_d)$ , it does not explicitly describe how to choose them in order to make the matrix in (15)  $\mathcal{R}$ -unimodular. However, from (14) and equivalently (15), the conditions in Theorem 2.3.1 below on the plant  $P$  are *necessary* for existence of decentralized controllers which reliably stabilize  $\mathcal{S}(F_S, P, F_A, C)$ . By Theorem 2.3.1, to achieve reliable decentralized stabilization,  $P_{12}$  and  $P_{21}$  are necessarily strongly  $\mathcal{R}$ -stabilizable. An LTI system  $\hat{P}$  is said to be strongly  $\mathcal{R}$ -stabilizable if there is an  $\mathcal{R}$ -stable  $\mathcal{R}$ -stabilizing controller  $C \in \mathcal{M}(\mathcal{R})$  for  $\hat{P}$  (in the standard full-feedback system). If  $U = \mathbf{C}_+$ ,  $\hat{P}$  is strongly  $\mathcal{R}$ -stabilizable if and only if it satisfies the *parity interlacing property*, i.e.,  $\hat{P}$  has an even number of poles between pairs of blocking zeros on the positive real-axis ([8], [9]). From a coprime factorizations view-point,  $\hat{P}$  is strongly  $\mathcal{R}$ -stabilizable if and only if, for any RCF  $(N_P, D_P)$  of  $\hat{P}$ , there exists an  $\mathcal{R}$ -unimodular  $\tilde{D}$  such that  $\tilde{D} D_P + \tilde{N} N_P$  is  $\mathcal{R}$ -unimodular for some  $\mathcal{R}$ -stable  $\tilde{N}$ .

**2.3.1. Theorem (Necessary conditions for reliable decentralized stabilizability):** Let  $P \in \mathcal{R}^{n_o \times n_i}$  be as in (2). If there exists a decentralized controller  $C_d$  such that  $\mathcal{S}(F_S, P, F_A, C)$  is reliably stabilized, then *i)*  $(N_{12}, D_{22})$  is an RCF of  $P_{12}$  and  $P_{12}$  is strongly  $\mathcal{R}$ -stabilizable, and *ii)*  $(\tilde{D}_{22}, \tilde{N}_{21})$  is an LCF of  $P_{21}$  and  $P_{21}$  is strongly  $\mathcal{R}$ -stabilizable.  $\square$

From Theorem 2.3.1, reliable decentralized stabilization may not always be possible to achieve. We now

study special cases where there exist decentralized controllers achieving reliable stabilization.

*Reliable decentralized stabilization for stable plants:* Let the plant  $P$  be  $\mathcal{R}$ -stable; then an RCF of  $P$  is given by  $(P, I)$ . The decentralized controller  $C_d$  achieves reliable stabilization if and only if  $C_d = \text{diag}[C_1, C_2]$ , with

$$C_1 = (I - Q_1 (P_{11} - P_{12} Q_2 P_{21}))^{-1} Q_1, \\ C_2 = (I - Q_2 P_{22})^{-1} Q_2, \quad (16)$$

where  $Q_1, Q_2 \in \mathcal{M}(\mathcal{R})$  are such that

$$I + Q_2 P_{21} Q_1 P_{12} \text{ is } \mathcal{R}\text{-unimodular,} \quad (17)$$

$$(I - Q_1 (P_{11} - P_{12} Q_2 P_{21})) \text{ is biproper,} \\ (I - Q_2 P_{22}) \text{ is biproper} \quad (18)$$

*Reliable decentralized stabilization for lower- or upper-triangular plants:* From (2), the plant  $P$  is lower-triangular (upper-triangular) if and only if  $N_{12} = 0$  ( $\tilde{N}_{21} = 0$ , respectively). In either case, from (14), reliable stabilization can be achieved if and only if  $D_{22}$  is  $\mathcal{R}$ -unimodular, equivalently,  $P$  is  $\mathcal{R}$ -stable. Hence,  $C_d$  achieves reliable stabilization if and only if it is given by (16), where  $Q_1, Q_2 \in \mathcal{M}(\mathcal{R})$  are such that (18) holds; note that (17) is automatically satisfied since either  $P_{12} = 0$  or  $P_{21} = 0$ .

*Reliable decentralized stabilization when  $P_{22}$  is strongly  $\mathcal{R}$ -stabilizable:* Let  $P_{22}$  be strictly proper and strongly  $\mathcal{R}$ -stabilizable. Suppose that  $P_{12}$  and  $P_{21}$  are square and invertible. A sufficient condition for decentralized reliable stabilization is that  $P_{22}$  is strongly  $\mathcal{R}$ -stabilizable, and in addition,  $P_{12}^{-1} = D_{22} N_{12}^{-1}$  and  $P_{21}^{-1} = \tilde{N}_{21}^{-1} \tilde{D}_{22}$  are  $\mathcal{R}$ -stable, i.e.,  $N_{12}$  and  $\tilde{N}_{21}$  are  $\mathcal{R}$ -unimodular. In this case, let  $C_S$  be any  $\mathcal{R}$ -stable  $\mathcal{R}$ -stabilizing controller for  $P_{22}$ . Without loss of generality, we can assume that the RCF  $(N_{22}, D_{22})$  of  $P_{22}$  is such that  $D_{22} + C_S N_{22} = I_{ni}$  and hence,

$$\begin{bmatrix} I & C_S \\ -N_{22} & I - N_{22} C_S \end{bmatrix} \begin{bmatrix} D_{22} & -C_S \\ N_{22} & I \end{bmatrix} = I. \quad (19)$$

Then for some  $A \in \mathcal{M}(\mathcal{R})$ ,  $\tilde{U}_{22}$  in (7) is  $\tilde{U}_{22} = (C_S + D_{22} A)$ . A reliable decentralized controller is given by  $C_d = \text{diag}[C_1, C_2]$ , where  $C_2$  is given by (8) with  $Q_2 = -A$  and  $C_1$  is given by (10) with  $Q_1 = \tilde{N}_{21}^{-1} N_{22} N_{12}^{-1}$ .

Now with  $P_{22}$  strongly  $\mathcal{R}$ -stabilizable, suppose that  $P_{21}$  is square and invertible and  $P_{12} = M P_{22}$  for

some  $\mathcal{R}$ -unimodular matrix  $M$ . Then  $N_{12} = M N_{22}$ . These conditions are also sufficient for existence of reliable decentralized controllers. In this case, a controller similar to the one given above can be used, where  $Q_2 = -A$  and  $Q_1 = \tilde{N}_{21}^{-1} M^{-1}$ .

*Reliable decentralized stabilization when  $P_{22}^{-1}$  is strongly  $\mathcal{R}$ -stabilizable:* Suppose that  $P_{22}$ ,  $P_{12}$  and  $P_{21}$  are square and invertible. A sufficient condition for decentralized reliable stabilization is that  $P_{22}^{-1}$  is strongly  $\mathcal{R}$ -stabilizable, and in addition,  $P_{12}^{-1} = D_{22} N_{12}^{-1}$  and  $P_{21}^{-1} = \tilde{N}_{21}^{-1} \tilde{D}_{22}$  are  $\mathcal{R}$ -stable, i.e.,  $N_{12}$  and  $\tilde{N}_{21}$  are  $\mathcal{R}$ -unimodular. Since  $P_{22}^{-1}$  is strongly  $\mathcal{R}$ -stabilizable, there exists a  $Q_2 \in \mathcal{M}(\mathcal{R})$  such that  $(\tilde{U}_{22} + D_{22} Q_2)$  is  $\mathcal{R}$ -unimodular, where  $\tilde{U}_{22}$  satisfies (7). In this case, a reliable decentralized controller is given by  $C_d = \text{diag}[C_1, C_2]$ , where  $C_2$  is given by (8) with  $Q_2$  such that  $(\tilde{U}_{22} + D_{22} Q_2)$  is  $\mathcal{R}$ -unimodular and  $C_1$  is given by (10) with  $Q_1 = \tilde{N}_{21}^{-1} (\tilde{U}_{22} + D_{22} Q_2)^{-1} [-D_{22} + I] N_{12}^{-1}$ .

*Reliable decentralized stabilization when  $X P_{12} = P_{22}$  and  $P_{21} Y = P_{22}$ :* Let  $P_{22}$  be strictly proper and strongly  $\mathcal{R}$ -stabilizable. Suppose that there exist  $\mathcal{R}$ -stable matrices  $X$  and  $Y$  of appropriate dimensions such that  $X P_{12} = P_{22}$  (equivalently,  $X N_{12} = N_{22}$ ) and  $P_{21} Y = P_{22}$  (equivalently,  $\tilde{N}_{21} Y = N_{22}$ ). These conditions are also sufficient for existence of reliable decentralized controllers. Again, let  $C_S$  be any  $\mathcal{R}$ -stable  $\mathcal{R}$ -stabilizing controller for  $P_{22}$  and assume that the RCF  $(N_{22}, D_{22})$  of  $P_{22}$  is such that  $D_{22} + C_S N_{22} = I_{n_i}$  and hence, (19) holds. Then for some  $A \in \mathcal{M}(\mathcal{R})$ ,  $\tilde{U}_{22}$  in (7) is  $\tilde{U}_{22} = (C_S + D_{22} A)$ . A reliable decentralized controller is  $C_d = \text{diag}[C_1, C_2]$ , where  $C_2$  is given by (8) with  $Q_2 = -A$  and  $C_1$  is given by (10) with  $Q_1 = Y \hat{Q}_1 X$  and  $\hat{Q}_1$  is chosen as follows: Let  $k$  be any integer larger than  $\|C_S N_{22}\|$ ; then  $(I - (C_S N_{22})/k)^k$  is  $\mathcal{R}$ -unimodular. By the binomial expansion (see for example [9]),

$$\begin{aligned} & (I - (C_S N_{22})/k)^k \\ &= I - (C_S N_{22}) + \sum_{\ell=2}^k r_\ell (C_S N_{22})^\ell, \end{aligned}$$

where  $r_\ell$  are the binomial coefficients. Choose  $\hat{Q}_1$  as

$$\hat{Q}_1 = \sum_{\ell=2}^k r_\ell (C_S N_{22})^{\ell-2} C_S. \quad (20)$$

For this  $\hat{Q}_1$ , condition (15) is satisfied and hence, the system is reliably stabilized.

### 3. Conclusions

Reliable decentralized stabilization was considered using a factorization approach. It was shown that reliable stabilization can be achieved using two decentralized controllers only if  $P_{12}$  and  $P_{21}$  are strongly stabilizable. Decentralized controllers achieving reliable stabilization were proposed for plants, where  $P_{22}$  is also strongly stabilizable.

### References

- [1] C. A. Desoer and A. N. Gündes, "Algebraic theory of feedback systems with tow-input two-output plant and compensator," *Int. Journal of Control*, vol. 47, no. 1, pp. 33-51, 1988.
- [2] A. N. Gündes, "Reliable stabilization of linear plants using a two-controller configuration," *Systems and Control Letters*, to appear, 1994.
- [3] A. N. Gündes, "Stability of feedback systems with sensor or actuator failures: Analysis," *Int. Journal of Control*, vol. 56, no. 4, pp. 735-753, 1992.
- [4] K. D. Minto, K.D. and R. Ravi, New results on the multi-controller scheme for the reliable control of linear plants, *Proc. American Control Conference*, pp. 615-619, 1991.
- [5] D. D. Siljak, On reliability of control, *Proc. 17th IEEE Conference on Decision and Control*, pp. 687-694, 1978.
- [6] D. D. Siljak, Reliable control using multiple control systems, *Int. Journal of Control*, vol. 31, no. 2, 303-329, 1980.
- [7] X. L. Tan, D. D. Siljak and M. Ikeda, Reliable stabilization via factorization methods, *IEEE Trans. Automatic Control*, vol. 37, pp. 1786-1791, 1992.
- [8] M. Vidyasagar, *Control System Synthesis: A Factorization Approach*, Cambridge, MA: M.I.T. Press, 1985.
- [9] M. Vidyasagar and N. Viswanadham, Algebraic design techniques for reliable stabilization, *IEEE Trans. Automatic Control*, vol. 27, pp. 1085-1095, 1982.

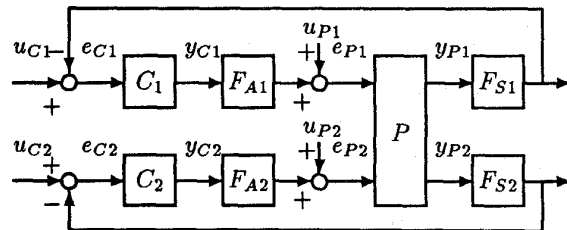


Figure 1: The system  $\mathcal{S}(P, C_d)$